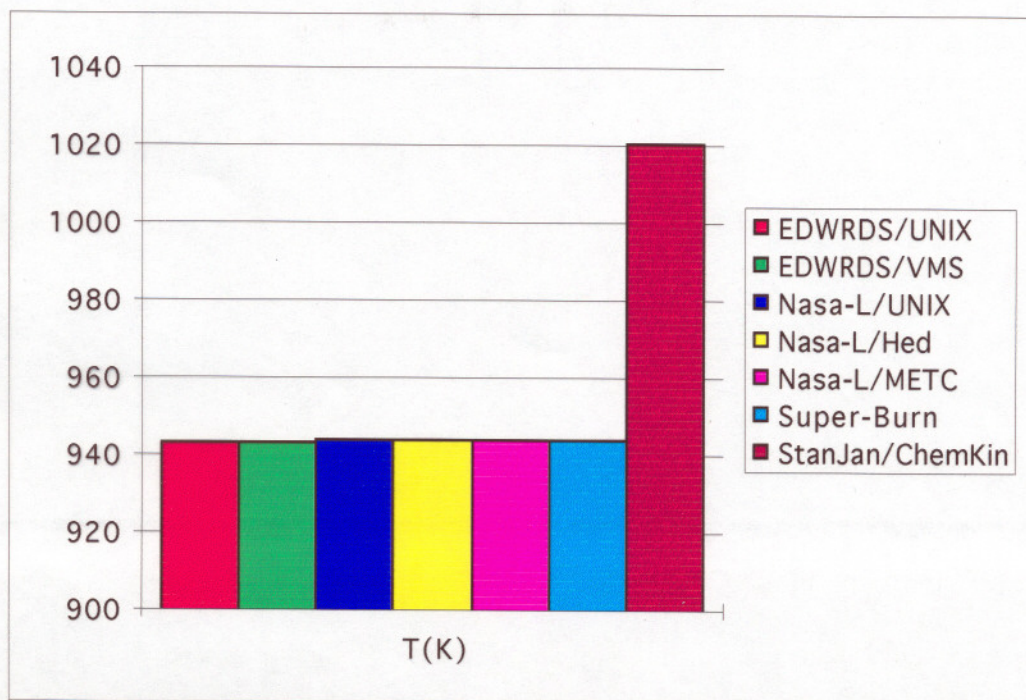
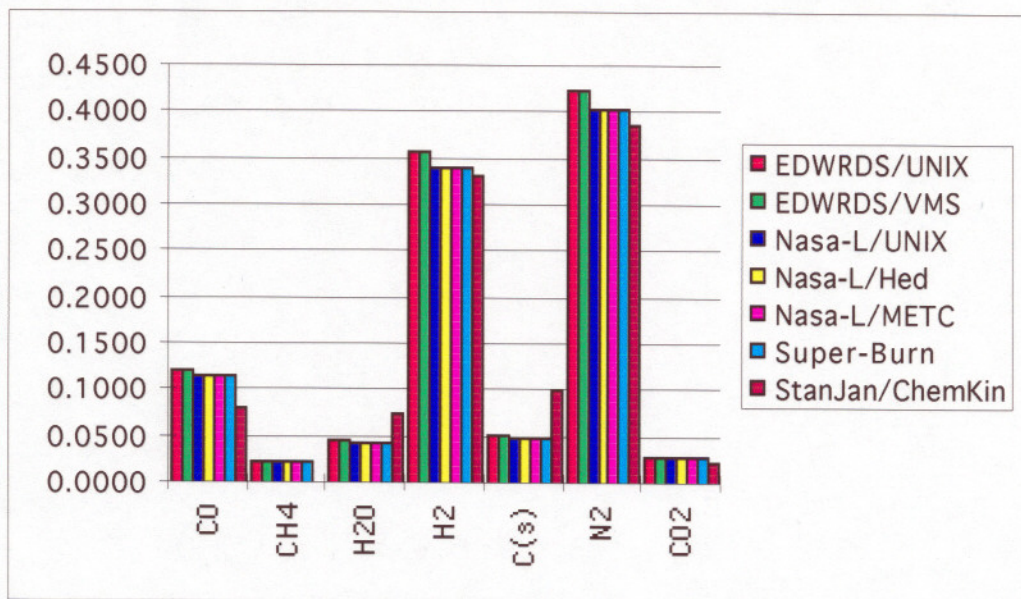
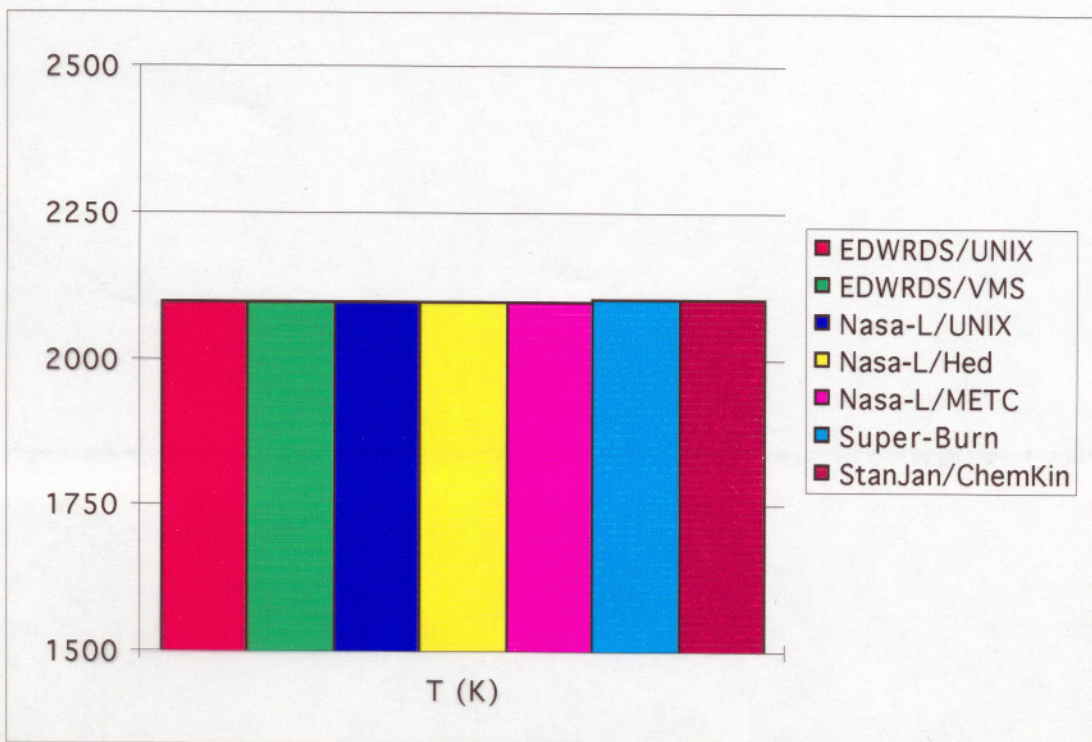
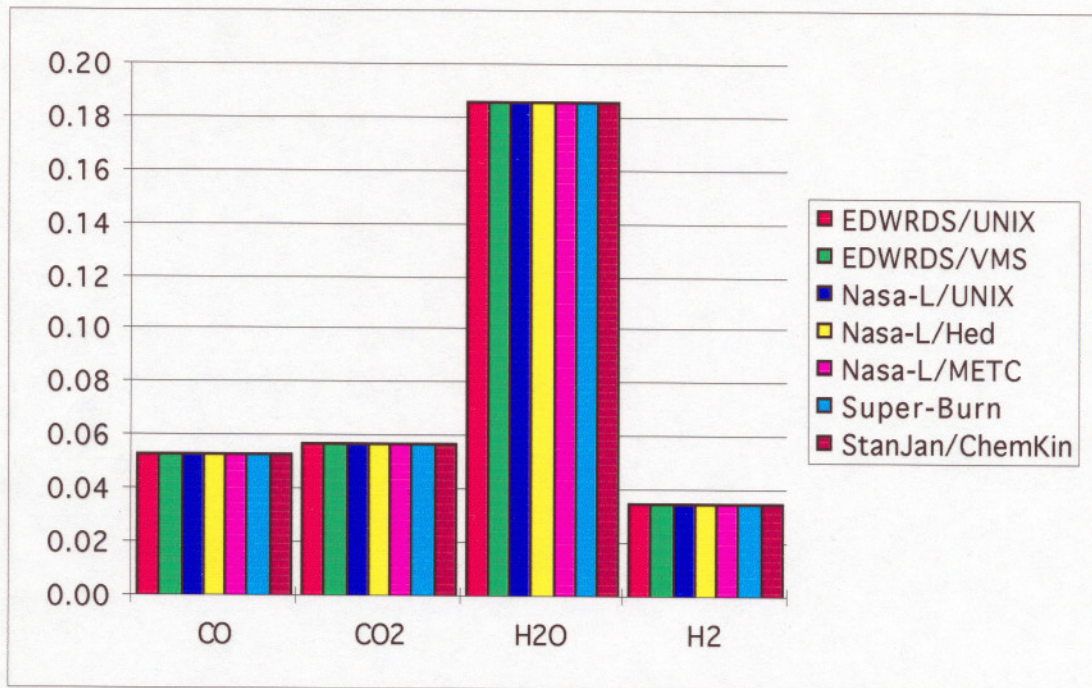


[illegible]

Case 3
CH₄/Air, Equiv. Ratio = 4.0
1 atm (HP Case)



Case 2
CH₄/Air, Equiv. Ratio = 1.25
1 atm (HP Case)



1. Hand ~~back~~ reports

2. Discuss Class

- partners
- workload
- weighting for 1st project
- schedule

3. What is Chemkin ; Why was it written?

- organized set of library subroutines to use with driver programs that use them ; multiple elementary reactions
- written so you only had to do it once, & not reinvent the wheel for every new code
- developed at Sandia CRF, but widely used!

4. Basic Chemkin package:

A. Interpreter

- 1. reads the reaction mechanism, elements, species
- 2. reads in additional thermo data (if needed)
- 3. writes the linking file

B. Thermodynamic Data Base

- minor modification to Nasa-Lewis data base

$$C_p = \left(\frac{\partial H}{\partial T} \right)_P$$

same

$$\left(\frac{\partial H}{\partial T} \right)_P = C_p$$

$$\frac{C_p^\circ}{R} = a_1 + a_2 T + a_3 T^2 + a_4 T^3 + a_5 T^4$$

$$\frac{H^\circ}{RT} = a_1 + \frac{a_2 T}{2} + \frac{a_3 T^2}{3} + \frac{a_4 T^3}{4} + \frac{a_5 T^4}{5} + \frac{a_6}{T}$$

$$\frac{S^\circ}{R} = a_1 \ln T + a_2 T + \frac{a_3}{2} T^2 + \frac{a_4}{3} T^3 + \frac{a_5}{4} T^4 + a_7$$

→ 2 temperature ranges

C. Linking file

- assembles the FORTRAN code : $C_p, h, \dots$

D. Gas-Phase Subroutine Library

subroutines that get values of $C_p, p, h, \dots$, etc.

given values of Y_i, P, T , etc.

Actually, $Y(1) = T$, $Y(2) = \text{Mass fraction of species 1}$

Chemkin History

- Developed at Sandia (Livermore, CA)
- Gained worldwide acceptance
- BYU got a copy
- Company formed to market the code

Reaction Design

www.reactiondesign.com

5. Convenient packages for "routine" analysis

we do not
have this!

A. Plug flow (1-D, no axial diffusion) (laminar)

B. Perfectly-stirred reactor (PSR)

C. Premixed 1-D laminar flame

* D. Surface reaction

E. Senkin

* F. Opposed jet

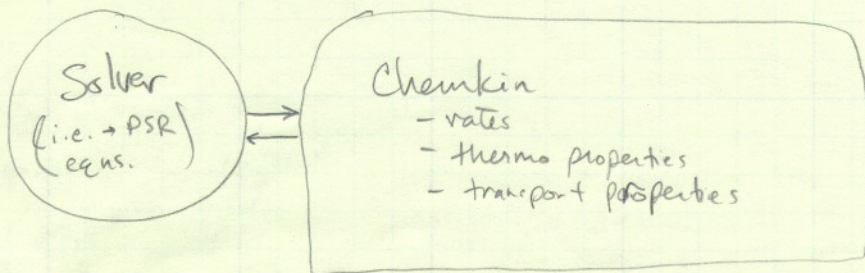
* G. Partially-stirred reactor (PaSR)

H. Equilibrium

I. Transport property look-up

* J. Plasmas

* Not to be studied in this class



6. Example:

A. Figure 2 (program schematic)

→ put in the reaction mechanism and inlet conditions

→ use the code that describes the right reactor (PSR, etc.)

B. Sample reaction set (overhead)

C. Sample problem: Batch reactor, constant P (like a CSTR under)

Overall continuity

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{v} = 0 \quad (= \dot{r}_{\text{solid} \rightarrow \text{gas}})$$

Species continuity

$$\frac{\partial \rho_i}{\partial t} + \nabla \cdot (\rho_i \mathbf{v} + \mathbf{j}_i) = \dot{r}_i \quad (\text{mass basis})$$

$$\frac{\partial \gamma_i \rho}{\partial t} = \gamma_i \frac{\partial \rho}{\partial t} + \rho \frac{\partial \gamma_i}{\partial t}$$

$$\nabla \cdot \gamma_i \rho \mathbf{v} = \gamma_i \nabla \cdot \rho \mathbf{v} + \rho \mathbf{v} \cdot \nabla \gamma_i$$

$$\gamma_i \frac{\partial \rho}{\partial t} + \rho \frac{\partial \gamma_i}{\partial t} + \gamma_i \nabla \cdot \rho \mathbf{v} + \rho \mathbf{v} \cdot \nabla \gamma_i + \nabla \cdot \mathbf{j}_i = \dot{r}_i$$

OR

$$\gamma_i \left(\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{v} \right) + \rho \left(\frac{\partial \gamma_i}{\partial t} + \mathbf{v} \cdot \nabla \gamma_i \right) + \nabla \cdot \mathbf{j}_i = \dot{r}_i$$

overall continuity

$$\rho \left(\frac{\partial \gamma_i}{\partial t} + \mathbf{v} \cdot \nabla \gamma_i \right) + \nabla \cdot \mathbf{j}_i = \dot{r}_i$$

no spatial derivatives in batch reactor

$$\boxed{\rho \frac{\partial \gamma_i}{\partial t} = \dot{r}_i}$$

mass fraction

molar production rate of k
MW

Chemkin example:

$$\frac{\partial \gamma_k}{\partial t} = \frac{\omega_k W_k}{\rho}$$

mass density

Energy

$$\rho C_p \frac{DT}{Dt} = -\nabla \cdot \mathbf{q} - \tau : \nabla \mathbf{v} + \sum_j j_j g_j + \left(\frac{\partial \ln V}{\partial T} \right)_{P, x_i} \frac{DP}{Dt}$$

$$\rho C_p \left(\frac{\partial T}{\partial t} + \mathbf{v} \cdot \nabla T \right) = + \sum_i H_i [\nabla \cdot \mathbf{J}_i - \dot{r}_i]$$

no spatial derivatives, adiabatic, ideal, no viscous or body forces

$$\boxed{\rho C_p \frac{\partial T}{\partial t} = - \sum_i H_i \dot{r}_i}$$

Chemkin example:

$$\frac{\partial T}{\partial t} = - \frac{1}{\rho C_p} \sum_k h_k \dot{w}_k W_k \leftarrow \text{MW}$$

$\uparrow$ mass heat capacity $\uparrow$ enthalpy of species k per unit mass

$\nwarrow$ molar production rate of species k

D. Show sample program

F_1 = energy eqn.

$F_2 \rightarrow F_{k+1}$ = species cont. eqns.

F = RHS of eqn. to be used in a solver!
(with a time step)

Advantage: "simple" to program if you know the system.

E. Show Igor plots

F. Note units:

$$P = \text{dynes/cm}^2$$

$$m = g$$

$$d = \text{cm}$$

$$E = \text{cal}$$

$$t = s$$

ELEMENTS

O H N

END

SPECIES

O O2 H H2 OH HO2 H2O H2O2

N2

END

REACTIONS

H+O2 = O+OH (MILLER 81)
H2+O = H+OH (MILLER 77)
H2+OH = H2O+H (DIXON-LEWIS 77)
OH+OH = H2O+O (COHEN 79)
H+OH+M = H2O+M (MILLER 77)
H2O /20.0/
O2+M = O+O+M (MILLER 81)
H2+M = H+H+M (MILLER 77)
H2O/6.0/ H/2.0/ H2/3.0/
H2+O2 = OH+OH (MILLER 77)
H+O2+M = HO2+M (SLACK 77)
H2O/21.0/ H2/3.3/ O2/0.0/ N2/0.0/
H+O2+O2 = HO2+O2 (SLACK 77)
H+O2+N2 = HO2+N2 (SLACK 77)
HO2+H = H2+O2 (LLOYD 74)
HO2+H = OH+OH (LLOYD 74)
HO2+O = OH+O2 (LLOYD 74)
HO2+OH = H2O+O2 (LLOYD 74)
HO2+HO2 = H2O2+O2 (TROE 69)
H2O2+M = OH+OH+M (BAULCH 72)
H2O2+H = HO2 + H2 (BAULCH 72)
H2O2+OH = H2O+HO2 (BAULCH 72)

END

$$k = A T^B e^{-E/RT}$$

A	B	E
5.1E16	-0.82	16510
1.8E10	1.0	8830
1.2E09	1.3	3630
6.0E08	1.3	0.0
7.5E23	-2.6	0.0
1.9E11	0.5	95560
2.2E12	0.5	92600
1.7E13	0.0	47780
2.1E18	-1.0	0.0
6.7E19	-1.42	0.0
6.7E19	-1.42	0.0
2.5E13	0.0	700
2.5E14	0.0	1900
4.8E13	0.0	1000
5.0E13	0.0	1000
2.0E12	0.0	0.0
1.2E17	0.0	45500
1.7E12	0.0	3750
1.0E13	0.0	1800

Figure 3. Example input file for the Chemkin Interpreter.

The Interpreter

Input of the reaction description to the Interpreter is designed to be essentially format-free and in familiar chemical notation. Nevertheless, there is still a certain syntax that must be followed. Some of the capabilities of the Interpreter are evident from the simple example input file shown in Fig. 3.

The first information that must be supplied to the Interpreter is about the chemical elements (or isotopes) that combine to form the species appearing in the reaction mechanism. The purpose of identifying the elements explicitly is to fix the order in which arrays of element information in the Gas-Phase Subroutine Library are referenced. For example, if a Chemkin subroutine were called to return an array of atomic weights for the elements they would be in exactly the same order in which they were presented to the Interpreter (e.g. if the atomic weights were stored in an array AWT, then in this example AWT(3) would be the atomic weight of the nitrogen). For the elements that appear on the periodic


```

SUBROUTINE FUN( NEQ, TIME, Y, F)
  DIMENSION Y(NEQ), F(NEQ)

C
C INPUT -
C   NEQ  - the number of dependent variables.
C   TIME - the independent variable, time.
C   Y    - the dependent variable vector (length NEQ), structured as:
C           y(1) = T, the temperature in Kelvins,
C           y(k+1) = Yk, the mass fraction of the kth species.
C OUTPUT -
C   F    - The righthand sides of the governing equations.
C -----
C
C   DIMENSION WT(10), H(10), WDOT(10)
C
C       These arrays are required to store output of some Chemkin
C       Subroutine calls. They allow for up to 10 species.
C       WT(*) - The molecular weights of the species (g/mole).
C       H(*) - The species enthalpies (erg/mole*K)
C       WDOT(*) - The species molar production rates (moles/cc*sec).
C -----
C
C   COMMON /CHEMKIN/ KK, P, IWORK(200), WORK(200)
C
C       This common block contains parameters and data that are needed,
C       but not available through the FUN call list.
C       KK - the number of species.
C       P - the pressure in dynes/cm**2
C       IWORK - the Chemkin integer work space.
C       WORK - the Chemkin real work space.
C
C   CALL CKRHOY( P, Y(1), Y(2), IWORK, WORK, RHO)
C   CALL CKCPBY( Y(1), Y(2), IWORK, WORK, CPB)
C   CALL CKHMS ( Y(1), IWORK, WORK, H)
C   CALL CKWYP ( P, Y(1), Y(2), IWORK, WORK, WDOT)
C   CALL CKWT ( IWORK, WORK, WT)
C
C       form the summation in eq. (6)
C   SUM=0.
C   DO 100 K=1, KK
C       SUM = SUM + H(K)*WDOT(K)*WT(K)
100 CONTINUE
C
C       form the righthand sides of eqs. (6) and (7)
C   F(1) = - SUM / (RHO*CPB)
C   DO 200 K=1, KK
C       F(K+1) = WDOT(K) * WT(K) / RHO
200 CONTINUE
C
C   RETURN
C   END

```

$$\begin{aligned}
 & \rho \quad C_p \quad h \quad \dot{w}_k \quad W_k \quad (MW's) \\
 & = \sum h_k \dot{w}_k W_k \\
 & = \frac{\sum h_k \dot{w}_k W_k}{\rho C_p} \\
 & = \frac{\dot{w}_k W_k}{\rho}
 \end{aligned}$$

Figure 4. Subroutine for defining governing equations for solution by LSODE.