

Lecture 7 - Conservation Equations

* Remember a few days ago, I said transport equations require two pieces:

- Constitutive Laws
- Balance Equations

* We have done constitutive laws in chapter 1. These laws are empirical and material specific. They give us relationships for fluxes.

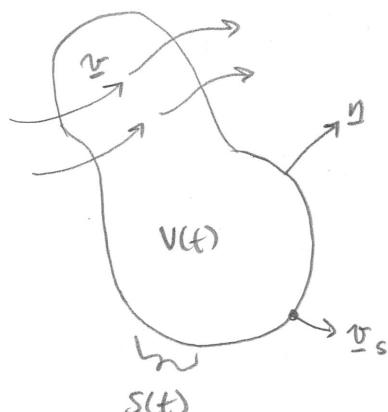
* We will now focus on balance equations. They are general & universal for conserved quantities.

* we will then combine the two together to get transport equations for:

- total mass
- species mass
- energy

I. General Balances

* Consider the following arbitrary control volume (c.v.)



$V(t)$: volume

$S(t)$: surface area

n : outward unit normal

v : fluid velocity

v_s : surface velocity (of c.v.)

* A c.v. is a mathematically defined region of study, like the "system" in thermo. It isn't magic, but a "smart" choice can simplify the problem.

+ We want to do a balance of some property, B , on the control volume. This is basically just accounting, but it's fancy because it can change in space and time.

(*) Note: This is a "general" balance because
 { it isn't specific to a single property. This abstraction can make it hard to understand.
 If it helps, imagine $B = \text{mass}$.

* Accounting Balance:

- accumulation = in - out + generation
- let $b(r, t)$ be the quantity B per volume at point r and time t in our C.V.

$$\text{accumulation} : \frac{d}{dt} \int_{V(t)} b(r, t) dV$$

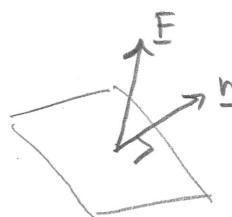
- let $B_v(r, t)$ be the rate of creation of B per unit volume

$$\text{generation} : \int_{V(t)} B_v(r, t) dV$$

- let \underline{F} be the total flux of B across the control surface.

(*) More about fluxes in a bit!

net rate of B in?



$$-\underline{n} \cdot \underline{F}$$

↑
outward unit normal

$$\underline{\text{in-out}} : - \int_{S(t)} \underline{n} \cdot \underline{E} d\underline{S}$$

- But wait, the surface can move. If it gets bigger (smaller) then we will add (subtract) $b(r,t)$ from the C.V.

- volumetric flow rate: $\underline{v}_s \cdot \text{Area}$

- in differential form: $\underline{n} \cdot \underline{v}_s d\underline{S}$

$$\underline{\text{in-out (2)}} : + \int_{S(t)} b(r,t) \underline{n} \cdot \underline{v}_s d\underline{S}$$

- Put it all together:

$$\frac{d}{dt} \int_{V(t)} b(r,t) dV = - \int_{S(t)} \underline{n} \cdot \underline{E} d\underline{S} + \int_{S(t)} b \underline{n} \cdot \underline{v}_s d\underline{S} + \int_{V(t)} B_r dV$$

* we can simplify this with Leibniz' rule (A.5-9, p. 623):

$$\frac{d}{dt} \int_{V(t)} b dV = \int_{V(t)} \frac{\partial b}{\partial t} dV + \int_{S(t)} b \underline{n} \cdot \underline{v}_s d\underline{S}$$

(how differentiate an integral)

- substitute into the LHS of the above & the $\underline{n} \cdot \underline{v}_s$ terms cancel

$$\int_{V(t)} \frac{\partial b}{\partial t} dV = - \int_{S(t)} \underline{n} \cdot \underline{E} d\underline{S} + \int_{V(t)} B_r dV$$

(1)

* Comments:

- General integral balance: sophisticated accounting
- Useful for "macroscopic analysis" (e.g. mechanical energy balances in fluids)

* We can use the general integral balance to get a general differential balance!

* Assume that $\underline{v}(t) = \underline{V}$ & $\underline{s}(t) = \underline{S}$. (This isn't strictly necessary, but it simplifies the derivation.)

* Recall Gauss' Divergence Theorem (A.5-2, p. 621)

$$\int_S \underline{n} \cdot \underline{F} d\underline{S} = \int_V \nabla \cdot \underline{F} dV$$

• Substitute into gen. integral balance

$$\int_V \frac{\partial b}{\partial t} dV = - \int_V \nabla \cdot \underline{F} dV + \int_V B_v dV$$

$$\Rightarrow \int_V \left[\frac{\partial b}{\partial t} + \nabla \cdot \underline{F} - B_v \right] dV = 0$$

\nwarrow volume is arbitrary, so the integrand must be zero.

$$\boxed{\frac{\partial b}{\partial t} = - \nabla \cdot \underline{F} + B_v} \quad (2)$$

* Comments:

- General differential balance: balance at every point in space
- PDE to solve for $b(\underline{r}, t)$
- Very general. Good for any scalar quantity, b , as long as the domain is continuous.

II. Example: conservation of total mass

* For total mass:

- $B = m \rightarrow b = \frac{m}{V} = \rho \leftarrow \text{density}$
- $\dot{E} = \rho \dot{V} \rightarrow \text{mass flux is equal to}$
 $\frac{\text{"mass flow rate"}}{\text{volume}}$
- $\nabla \cdot \mathbf{v} = 0 \rightarrow \text{no mass created or destroyed.}$

$$\frac{\partial b}{\partial t} = -\nabla \cdot \mathbf{F} + B \mathbf{v}$$

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \mathbf{v}) + \dot{\rho}$$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

"continuity
equation"

• Mass conservation at a point in space.

* A common simplification is $\rho = \text{const.}$

This simplifies continuity to :

$$\nabla \cdot \mathbf{v} = 0$$

"incompressible"
continuity Eq.

(Extra space b/c added this page)

III. Alternate Forms of the balances

- * The general balances have different forms they can be written in.
- * One way to write them involves dividing the total flux, \underline{F} , into a convective and diffusive part:

$$\underline{F} = b \underline{v} + \underline{f}$$

↑ ↑ ↑
 total flux convective diffusive flux
 flux

example: $\underline{n}_i = \underline{f}_i \underline{v} + \underline{j}_i$ $b = f_i$ ← species mass

↑ ↑ ↑
 total flux "mass flow rate" diffusive flux
 of i from Fick's law

(*) For total mass, $f_i = 0$.
No diffusive flux.

- * The diffusive flux is due to molecular motion causing transport.
- * The convective flux is due to bulk fluid flow carrying the property with it.
- * Subbing into our differential balance gives

$$\nabla \cdot \underline{F} = \nabla \cdot (b \underline{v}) + \nabla \cdot \underline{f}$$

$$\frac{\partial b}{\partial t} + \nabla \cdot (b \underline{v}) = - \nabla \cdot \underline{f} + B \underline{v}$$

(3)

- * Another way to write balances uses the material derivative:

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \underline{v} \cdot \nabla$$

- Rate of change seen by an observer moving with the fluid velocity (a material element)
- Same as a total derivative, with spatial derivatives set to fluid velocity:

$$\frac{d}{dt} = \frac{\partial}{\partial t} + \frac{\partial x}{\partial t} \frac{\partial}{\partial x} + \frac{\partial y}{\partial t} \frac{\partial}{\partial y} + \frac{\partial z}{\partial t} \frac{\partial}{\partial z}$$

(only write if they need to see it)

* We can write the general property balance using the material derivative as well:

$$\text{Eq 3: } \frac{\partial b}{\partial t} + \nabla \cdot (b \underline{v}) = - \nabla \cdot \underline{f} + B_v$$

$$\text{let } \hat{B} = \frac{b}{\rho} \Rightarrow b = \rho \hat{B} \leftarrow \text{"specific" B}$$

$$\frac{\partial}{\partial t} (\rho \hat{B}) + \nabla \cdot (\rho \hat{B} \underline{v}) = - \nabla \cdot \underline{f} + B_v$$

$$\underbrace{\hat{B} \left[\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{v}) \right]}_0 + \underbrace{\rho \left[\frac{\partial \hat{B}}{\partial t} + \underline{v} \cdot \nabla \hat{B} \right]}_{\frac{d\hat{B}}{dt}} = - \nabla \cdot \underline{f} + B_v$$

(continuity)

$\frac{d\hat{B}}{dt}$

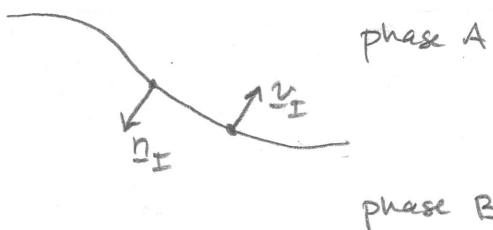
$$\boxed{\rho \frac{d\hat{B}}{dt} = - \nabla \cdot \underline{f} + B_v}$$

IV. Conservation Equations at Interfaces

* what happens if $b(r,t)$ is not continuous?

This happens at boundaries. Balances put a constraint on boundary conditions.

- * Special control volume that includes a boundary in it:



n_I : unit normal of interface (points to B by convention)

v_I : velocity of interface

B_s : generation at surface

F : total flux

- * Skipping a very similar derivation (see §2.2, p.31)
we get the equation:

$$\boxed{[(F - b\underline{v}_I)]_B - (F - b\underline{v}_I)_A \cdot n_I = B_s}$$

↑ ↑ ↑
 flux relative flux relative generation
 to the interface to the interface at the
 on the B side on the A side interface.

- * Using convective and diffusive fluxes, this can be written as:

$$\boxed{[(f + b(\underline{v} - \underline{v}_I))]_B - (f + b(\underline{v} - \underline{v}_I))_A \cdot n_I = B_s}$$

\underline{v} : fluid velocity , recall $F = b\underline{v} + f$