

Chemical Engineering 512

Nuclear Reactor Transient Modeling

Lecture 19

Reactor Kinetics



Spiritual Thought

D&C 121:41-42

41 No power or influence can or ought to be maintained by virtue of the priesthood, only by persuasion, by long-suffering, by gentleness and meekness, and by love unfeigned;

42 By kindness, and pure knowledge, which shall greatly enlarge the soul without hypocrisy, and without guile—”



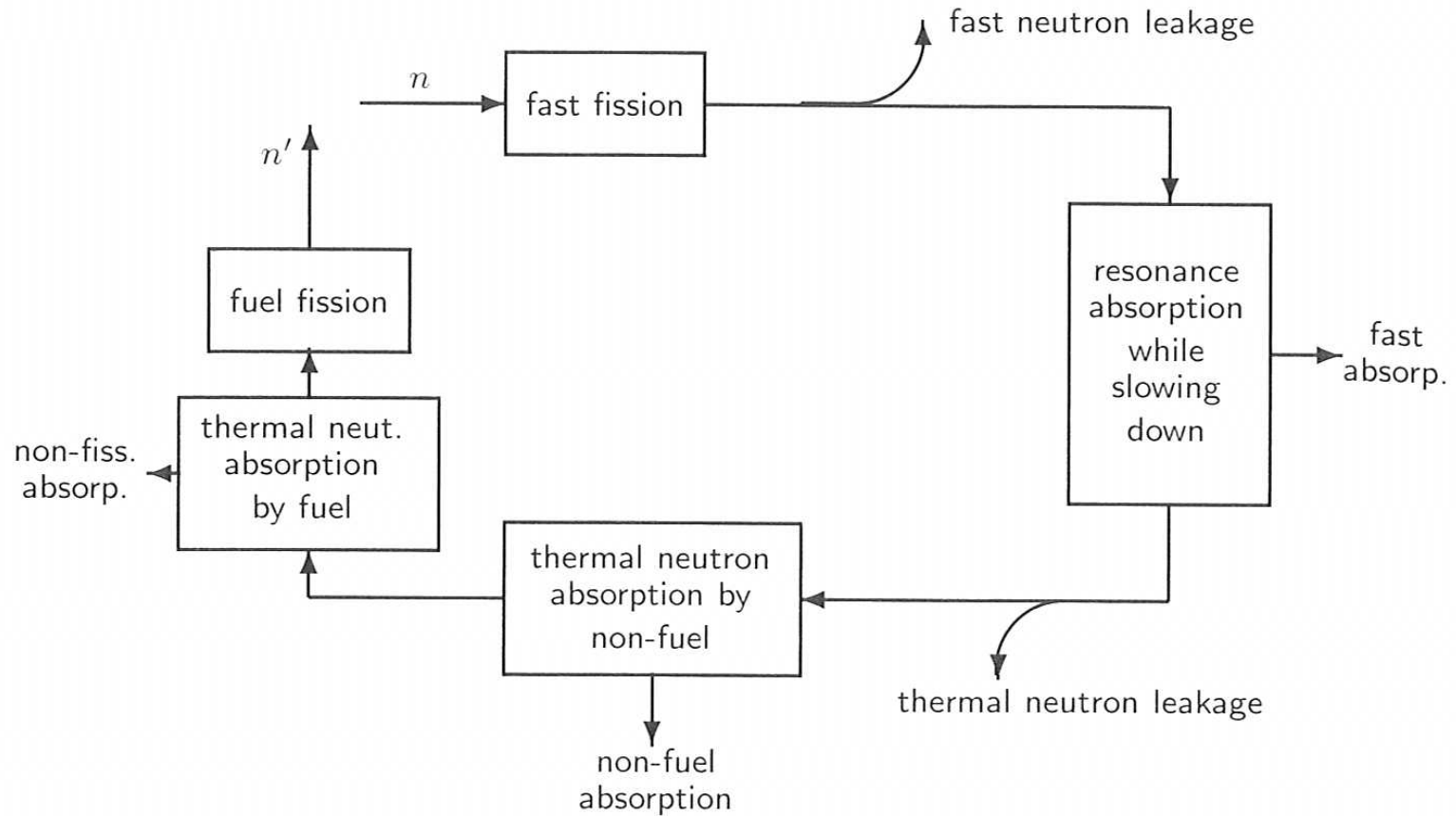
Objectives

- Learn basics of reactor kinetics
- Learn how to input kinetics into RELAP5-3D
- Practice inputting kinetics into RELAP5-3D
- Talk about how to apply this to an existing RELAP5-3D model



Fast Neutron Life Cycle

- What happens to fast neutrons?



Multiplication Factor

$$k_{eff} \equiv \frac{\text{neutrons at point in cycle}}{\text{neutrons at same point in previous generation}}$$

$$k_{eff} = \frac{n'}{n}$$

$$k_{eff} = \epsilon p \eta f P_{NL}^f P_{NL}^{th}$$



Reactivity and Worth

$$\rho \equiv \frac{k_{eff} - 1}{k_{eff}} = \frac{\delta k}{k_{eff}} \quad \text{reactivity } \rho \text{ and } \delta k$$

$$k(\$) \equiv \frac{\rho}{\beta} \quad \begin{array}{l} \beta \text{ is delayed neutron fraction} \\ \text{worth can be measured in units of } k(\$) \text{ or } k \end{array}$$

- cents?
- Percent Mil?



Delayed Neutrons

TABLE 3.5 DELAYED NEUTRON DATA FOR THERMAL FISSION IN $^{235}\text{U}^*$

Group	Half-Life (sec)	Decay Constant (λ_i , sec^{-1})	Energy (ke V)	Yield, Neutrons per Fission	Fraction (β_i)
1	55.72	0.0124	250	0.00052	0.000215
2	22.72	0.0305	560	0.00346	0.001424
3	6.22	0.111	405	0.00310	0.001274
4	2.30	0.301	450	0.00624	0.002568
5	0.610	1.14	—	0.00182	0.000748
6	0.230	3.01	—	0.00066	0.000273

Total yield: 0.0158

Total delayed fraction (β) 0.0065

*Based in part on G. R. Keepin, *Physics of Nuclear Kinetics*, Reading, Mass.: Addison-Wesley, 1965.

For 1-group model, $T_{\frac{1}{2}}$ for ^{235}U is about 8.87 s and τ is about 12.8 s.



Simple Kinetics Model

$$\Delta n(t) \equiv \ell_p \frac{dn(t)}{dt} = (k_{eff} - 1)n(t)$$

$$\frac{dn(t)}{dt} = \frac{k_{eff} - 1}{\ell_p} n(t)$$

$$\Rightarrow n(t) = n(0) \exp\left(\frac{k_{eff} - 1}{\ell_p} t\right)$$

- For ^{235}U
 - $\ell_p = 2.1 \times 10^{-4} \text{ s}$
 - $k_{eff} - 1 = 0.001$
 - and $t = 1 \text{ s}$,
- $n/n^0 = 117$ (22,027 if $\ell' = 10^{-4}$ as in text)
- Far too rapid to control!!!



Reactors with delayed neutrons

Delayed neutrons: β is fraction of total neutrons

$$\bar{\ell}_p = (1 - \beta)\ell_p + \beta(\ell_p + \tau) \approx \ell_p + \beta\tau$$

τ is lifetime of delayed neutrons $= \frac{T_{1/2}}{\ln 2} \approx 12.8 \text{ s}$

For $\delta k \ll \beta$

$$\frac{n(t)}{n_0} = \exp\left(\frac{k_{eff} - 1}{\bar{\ell}_p}\right) = \exp\left(\frac{t}{T}\right)$$
$$T = \frac{\bar{\ell}_p}{k_{eff} - 1} = \frac{\beta\tau}{\delta k}$$

- For ^{235}U , $T = 83 \text{ s}$, $k_{eff} - 1 = 0.001$,
- $n/n^0 = 1.012$
- This can be controlled!



Reactivity Equation Solutions

$$T = \frac{\bar{l}}{k_{eff} - 1} = \frac{\bar{l}}{\delta k} = \frac{\beta\tau}{\delta k} =$$

Reactor period - The time required for a neutron population to change by a factor of e

$$k_{eff} = 1 + \delta k = 1 + \frac{\beta\tau}{T}$$

τ = Lifetime of delayed neutrons
~12.8s (U235)

$$T = \frac{\beta\tau}{\delta k} = \frac{\beta\tau}{k_{eff} - 1} = \frac{\beta\tau}{k_{eff}\rho} = \frac{\tau}{k_{eff}\rho(\$)} \approx \frac{\tau}{\rho(\$)}$$

$$\phi(t) = \exp\left(\frac{t}{T}\right)$$

Remember, Flux is proportional to power....

$$C \cdot P(t) = \exp\left(\frac{t}{T}\right) \quad \frac{t}{T} = \exp\left(\frac{P(t) \cdot C}{P(0) \cdot C}\right) \quad \frac{t}{T} = \exp\left(\frac{P(t)}{P(0)}\right)$$



Power Changes

$$T = \frac{\beta\tau}{\delta k} = \frac{\beta\tau}{keff \cdot \rho} = \frac{\tau}{keff \cdot k(\$)} \sim \frac{\tau}{k(\$)}$$

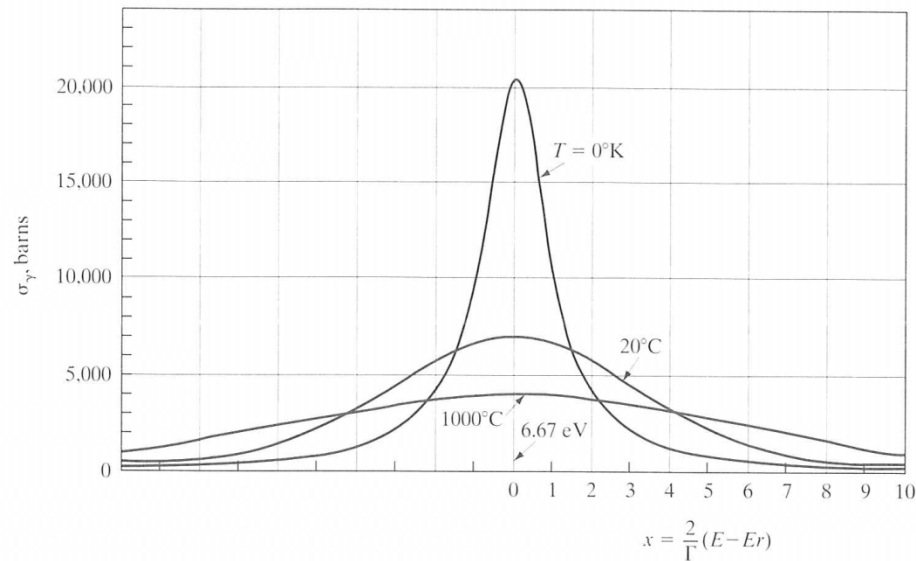
- T = Reactor Period (units of time)
 - Time required to increase reactor power (or neutron flux) by 2.72
- Integrate solution with specific values (initial time power to final time/power)

$$\frac{t}{T} = \ln \left[\frac{P(t)}{P(0)} \right]$$



Temperature Dependence

$$\alpha_T = \frac{d\rho}{dT} = \frac{d}{dT} \left(\frac{k-1}{k} \right) = \frac{1}{k^2} \frac{dk}{dT} \cong \frac{1}{k} \frac{dk}{dT}$$



Breit-Wigner describes absorption profile at 0 K but Doppler effect broadens peaks, with little change in area, at higher temperatures.

$$\sigma_\gamma(E) = \frac{\lambda_r^2 g}{4\pi} \frac{\Gamma_n \Gamma_\gamma}{(E - E_r)^2 + \frac{\Gamma^2}{4}}$$

- α_T = temperature reactivity feedback coefficient
- If $\alpha_T > 0$,
 - Unstable
 - increases and decreases in temperature run away to meltdown or shutdown without operator response.
- If $\alpha_T < 0$,
 - Stable
 - Increases and decreases in temperature self regulate and the reactor stabilizes.
- Different α 's for fuel/moderator
 - Different timescales
 - Fuel is most rapid
 - α_{prompt}
- NRC requires negative α_{prompt} values for licenses

Feedback Types

- Flowering
- Axial Expansion
- Radial Expansion
- Coolant
- Doppler



Kinetics Type

Point

- Core-average fluid conditions, weighting factors, feedback coefficients are used
- Power distribution does not change with time
- Can perform quick calculations

Nodal

- Initial conditions calculated by model and are nodalized
- Power distribution is calculated based on time
- Takes much longer to calculate these equations yet leads to more realistic results



Feedback Type

Separable

- Moderator Density
 - Moderator Temperature
 - Fuel Temperature
-
- Changes in one of these DO NOT effect the others

Table

- Moderator Density
 - Moderator Temperature
 - Fuel Temperature
-
- Changes in these DO effect each other



Kinetics RELAP Input Cards

- 30000000 – Type Card
- 30000001 – Reactor Kinetics Information
- 30000002 – Fission Product Decay Information
- 300004NN – Power History Data



30000000 – Type Card

- $W1(A)$ – Kinetics Type (nodal or point)
- $W2(A)$ – Feedback Type



300000001 – Reactor Kinetics Information

- W1(A) – Fission product decay type
- W2(R) – Total reactor power
- W3(R) – Initial reactivity
- W4(R) – Delayed neutron fraction over prompt neutron lifetime
- W5(R) – Fission product yield factor
- W6(R) – ^{239}U yield factor
- W7(R) – Fissions per initial fissile atom
- W8(R) – Reactor operating time
- W9(R) – Units for W8



- W1(A) – Fission product type
- W2(R) – Energy release per fission
- W3-W10 – As needed based upon W1



300004NN – Power History Data

- W1(R) – Reactor power
- W2(R) – Time duration
- W3(A) – Time duration units
- If not inputted, infinite operation at previously input total reactor power is assumed.



Separable Option

- 300005NN Desnity Reactivity Table
 - W1 – Modertor Density
 - W2 – Reactivity
- 300006NN Doppler Reactivity Table
 - W1 Fuel Temperature
 - W2 – Reactivity



Example

- Download Lecture 22.i
- Fill in the blanks based upon the following
 - Kinetics Type - Separable
 - Delayed Neutron Fraction (β) – 0.0056
 - Prompt neutron lifetime – 0.000025s
 - Doppler reactivity coefficient – $((-0.0000158^{\circ}\text{F}^{-1})/\beta) * (\Delta T)$
 - Moderator Density Reactivity
 - Convert reactivity to \$
 - Hint: \$ = $\%/\beta$

Density (lb/ft ³)	Reactivity (%)
4.7	-68.5
14.0	-30.0
23.4	-14.1
35.1	-4.8
46.8	0.0
56.2	3.0



Answer

```

7      *      KineticsType      FeedbackType
8      30000000 point      separabl
9      *
10     30000001 gamma-ac 3600.e6 0.0 224.0 1.0 0.48
11     *      Type
12     30000002 ans79-1
13     *      Table/ContVarNum
14     30000011 2
15     *      Denisty Reactivity Table
16     *      ModeratorDensity      Reactivity
17     30000501 4.7 -122.3
18     30000502 14.0 -53.6
19     30000503 23.4 -25.2
20     30000504 35.1 -8.57
21     30000505 46.8 0.0
22     30000506 56.2 5.36
23     *      Doppler Reactivity Table
24     *      Temperature      Reactivity
25     30000601 200. 5.08
26     30000602 2000. 0.0
27     30000603 5000. -8.46
28     *
29

```



Connecting To a Heat Structure

```

278 *****
279 *
280 *                               Heat Structures
281 *
282 *****
283 *
284 *      AxialHS  RadMesh  GeoType  SSFlag  LeftBound  Reflood
285 11000000      6        8         2        1         5.74        0
286 *      MeshLocation      MeshFormat
287 11000100      0         1
288 *      NumOfIntervals      RightCoordinate
289 11000101      7         6.5
290 *      CompositionNum      IntervalNum
291 11000201      5         7
292 *      CompositionNum      IntervalNum
293 11000301      1000.        7
294 *      InitialTemp      MeshPointNum
295 11000401      500.        8
296 *      BoundaryVol/Table  Incr  BCType  SACode  SA/Factor  HSNum
297 11000501      150010000      0        1        1        10.0        6
298 *      BoundaryVol/Table  Incr  BCType  SACode  SA/Factor  HSNum
299 11000601      0            0        0        1        10.0        6
300 *      SourceType  Pf      LeftBoundMult  RightBoundMult  HSNum
301 11000701      1000      0.001791  0.0            0.0            6
302 *      WordFormat
303 11000800      0
304 *      HydDiam  HLFor  HLRev  GSLFor  GSLRev  GLCFor  GLCRev  Boil  HSNum
305 11000801      0.0      3.0      3.0      0.0      0.0      0.0      0.0      1.0  6
306 *      WordFormat
307 11000900      0
308 *      HydDiam  HLFor  HLRev  GSLFor  GSLRev  GLCFor  GLCRev  Boil  HSNum
309 11000901      0.0      3.0      3.0      0.0      0.0      0.0      0.0      1.0  6
310 *

```



Assignment

- Homework 10 Due 11/14/23

