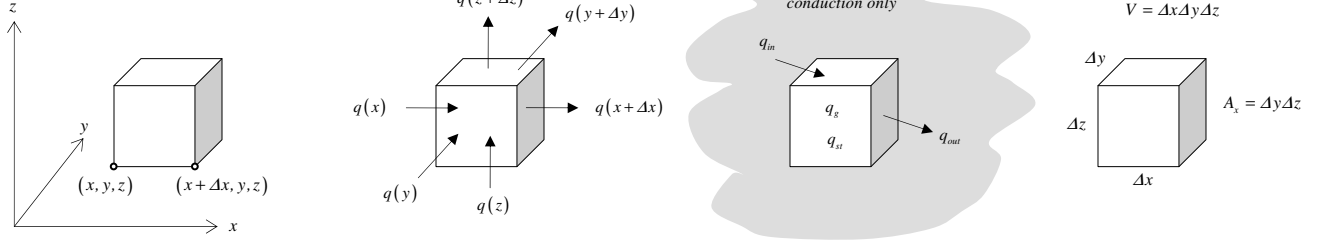


THE HEAT EQUATION

Derivation of the Heat Equation in the Cartesian coordinates (finite control volume approach)

Consider a Control Volume
in the stagnant continuous medium



Energy Balance:

$$q_{in} - q_{out} + q_g = q_{st}$$

$$q(x) - q(x + \Delta x) + q(y) - q(y + \Delta y) + q(z) - q(z + \Delta z) + q_g = q_{st}$$

$$\begin{aligned} q_x &= q_x'' \cdot A_x = q_x'' \cdot \Delta y \cdot \Delta z \\ q_y &= q_y'' \cdot A_y = q_y'' \cdot \Delta x \cdot \Delta z \\ q_z &= q_z'' \cdot A_z = q_z'' \cdot \Delta x \cdot \Delta y \end{aligned}$$

$$[q''(x) - q''(x + \Delta x)]\Delta y \Delta z + [q''(y) - q''(y + \Delta y)]\Delta x \Delta z + [q''(z) - q''(z + \Delta z)]\Delta x \Delta y + \dot{q} \Delta x \Delta y \Delta z = \rho c_p \frac{\partial T}{\partial t} \Delta x \Delta y \Delta z$$

divide equation
by $\Delta x \Delta y \Delta z$

$$-\frac{q''(x + \Delta x) - q''(x)}{\Delta x} - \frac{q''(y + \Delta y) - q''(y)}{\Delta y} - \frac{q''(z + \Delta z) - q''(z)}{\Delta z} + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

take a limit when
 $\Delta x \rightarrow 0$
 $\Delta y \rightarrow 0$
 $\Delta z \rightarrow 0$

$$-\frac{\partial q_x''}{\partial x} - \frac{\partial q_y''}{\partial y} - \frac{\partial q_z''}{\partial z} + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

apply Fourier's Law:

$$\begin{aligned} q_x'' &= -k \frac{\partial T}{\partial x} \\ q_y'' &= -k \frac{\partial T}{\partial y} \\ q_z'' &= -k \frac{\partial T}{\partial z} \end{aligned}$$

$$\frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

In general, k is a tensor with components:

$$\begin{aligned} k_x(T) \\ k_y(T) \\ k_z(T) \end{aligned}$$

depending on temperature

assume :
 $k = \text{const}$

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{\rho c_p}{k} \frac{\partial T}{\partial t}$$

introduce :
 $\alpha = \frac{k}{\rho c_p}$

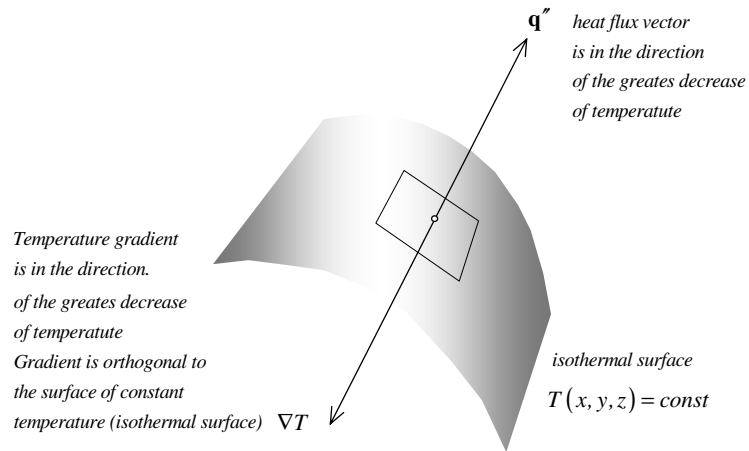
$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

The Heat Equation

$$T(x), \dot{q}(x)$$

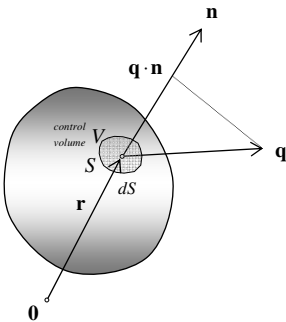
FOURIER'S LAW

$$\mathbf{q}'' = -k \nabla T$$



The Heat Equation - Derivation Consider a point in the system defined by a position vector $\mathbf{r} \in D \subset \mathbb{R}^3$. Let V be an arbitrary small control volume containing the point $\mathbf{r}$.

Conservation of energy principle for control volume V :



$$\left[\begin{array}{c} \text{rate of} \\ \text{net heat flow} \\ \text{through the} \\ \text{boundary } S \end{array} \right] + \left[\begin{array}{c} \text{rate of heat} \\ \text{generation} \\ \text{in volume } V \end{array} \right] = \left[\begin{array}{c} \text{rate of heat} \\ \text{storage} \\ \text{in volume } V \end{array} \right]$$

$$-\int_S \mathbf{q}(\mathbf{r}, t) \cdot \mathbf{n} dS + \int_V g(\mathbf{r}, t) dV = \int_V \rho c_p \frac{\partial T(\mathbf{r}, t)}{\partial t} dV$$

Apply the divergence theorem and combine the terms:

$$\int_V \left[-\nabla \cdot \mathbf{q}(\mathbf{r}, t) + g(\mathbf{r}, t) - \rho c_p \frac{\partial T(\mathbf{r}, t)}{\partial t} \right] dV = 0$$

Because V is an arbitrary control volume, in the limit when $V \rightarrow 0$:

$$-\nabla \cdot \mathbf{q}(\mathbf{r}, t) + g(\mathbf{r}, t) - \rho c_p \frac{\partial T(\mathbf{r}, t)}{\partial t} = 0$$

Apply the Fourier Law:

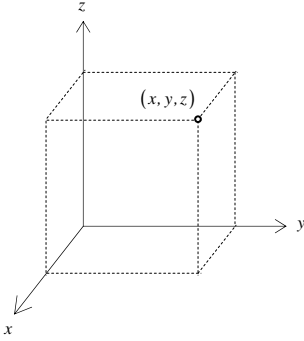
$$\nabla \cdot [k(\mathbf{r}) \nabla T(\mathbf{r}, t)] + g(\mathbf{r}, t) = \rho(\mathbf{r}) c_p(\mathbf{r}) \frac{\partial T(\mathbf{r}, t)}{\partial t}$$

If k, ρ, c_p are constant, then

$$\nabla^2 T(\mathbf{r}, t) + \frac{g(\mathbf{r}, t)}{k} = \frac{1}{\alpha} \frac{\partial T(\mathbf{r}, t)}{\partial t}$$

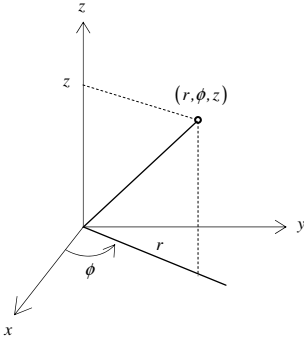
Vector form

$$\nabla^2 T(\mathbf{r}, t) + \frac{g(\mathbf{r}, t)}{k} = \frac{1}{\alpha} \frac{\partial T(\mathbf{r}, t)}{\partial t}$$

Cartesian coordinates

$$\nabla T = \left\langle \frac{\partial T}{\partial x}, \frac{\partial T}{\partial y}, \frac{\partial T}{\partial z} \right\rangle$$

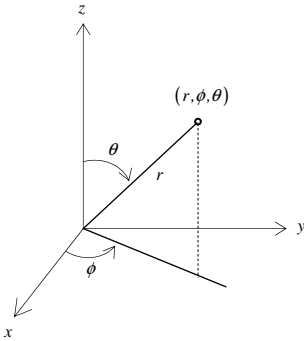
$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t} \quad (2.21)$$

Cylindrical coordinates

$$\nabla T = \left\langle \frac{\partial T}{\partial r}, \frac{1}{r} \frac{\partial T}{\partial \phi}, \frac{\partial T}{\partial z} \right\rangle$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \phi^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t} \quad (2.26)$$

$$r \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial r^2} + \frac{1}{r^2} \frac{\partial^2 T}{\partial \phi^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

Spherical coordinates

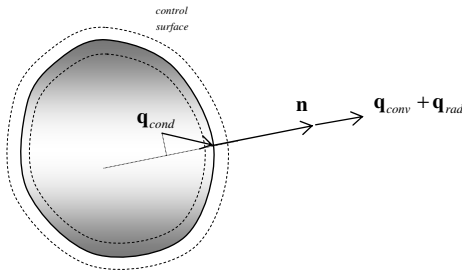
$$\nabla T = \left\langle \frac{\partial T}{\partial r}, \frac{1}{r \sin \theta} \frac{\partial T}{\partial \phi}, \frac{1}{r} \frac{\partial T}{\partial \theta} \right\rangle$$

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t} \quad (2.29)$$

$$\frac{2}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial r^2} + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

Derivation of the Boundary Condition

Energy balance for Control Surface:



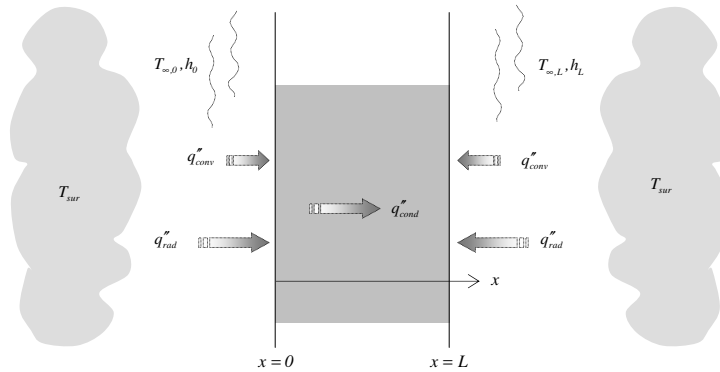
$$\mathbf{q}_{cond}(\mathbf{r}, t) \cdot \mathbf{n}|_S = h[T(\mathbf{r}, t)|_S - T_\infty] + \varepsilon \sigma [T^4(\mathbf{r}, t)|_S - T_{sur}^4]$$

2.4

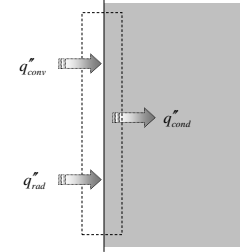
BOUNDARY CONDITIONS

in 1-D Cartesian Coordinates

Consider the boundaries $x = 0$ and $x = L$ exposed to convective and radiative environment



Energy Balance for Control Surface:



Energy Balance:

$$q_{cond}'' = q_{conv}'' + q_{rad}''$$

$$\left[-k \frac{dT}{dx} \right]_{x=0} = h[T_\infty - T(0)] + \varepsilon \sigma [T_{sur}^4 - T^4(0)]$$

non-linear boundary condition

$$\left[-k \frac{dT}{dx} + hT \right]_{x=0} = hT_\infty$$

linear convective boundary condition with $h = h_{conv} + h_{rad}$ effective convective coefficient when it is assumed that $T_{sur} = T_\infty$

Linearization of the boundary conditions:

$$\begin{aligned} \varepsilon \sigma [T_{sur}^4 - T^4(0)] &= \varepsilon \sigma [T_{sur}^2 + T^2(0)] [T_{sur} + T(0)] [T_{sur} - T(0)] \\ &= h_{rad} [T_{sur} - T(0)] \end{aligned}$$

$$h_{rad} = \varepsilon \sigma [T_{sur}^2 + T^2(0)] [T_{sur} + T(0)]$$

$$\text{if } \frac{|T - T_{sur}|}{T_{sur}} \ll 1 \text{ then } h_{rad} \approx 4\varepsilon \sigma T_{sur}^3$$

Dirichlet	I	$[T]_{x=0} = T_{s,0}$	$[T]_{x=L} = T_{s,L}$	prescribed temperature at the boundary (thermostated boundary with the surface temperature $T_s = T_\infty$ when $h \gg k$)
Neumann	II	$\left[-k \frac{dT}{dx} \right]_{x=0} = q_{s,0}''$	$\left[k \frac{dT}{dx} \right]_{x=L} = q_{s,L}''$	prescribed heat flux at the boundary $\left[\frac{dT}{dx} \right]_{x=0} = 0$ insulated boundary when $k \gg h$
Robin	III	$\left[-k \frac{dT}{dx} + h_0 T \right]_{x=0} = h_0 T_{\infty,0}$	$\left[k \frac{dT}{dx} + h_L T \right]_{x=L} = h_L T_{\infty,L}$	convective boundary condition

INITIAL CONDITION

$$T(x, y, z, 0) = T_0(x, y, z)$$

for all interior points of the domain $(x, y, z) \in D$