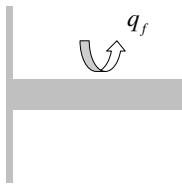


FIN PERFORMANCE

Single Fin



A_f = fin area

$$\eta_f = \frac{q_f}{q_{max}} = \frac{q_f}{h(T_b - T_\infty) A_f}$$

definition of fin efficiency

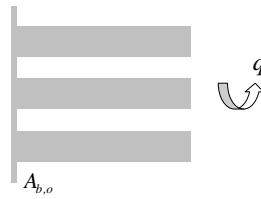
$$q_f = \frac{T_b - T_\infty}{R_{t,f}}$$

rate of heat transfer from a fin

$$R_{t,f} = \frac{I}{hA_f \eta_f}$$

fin thermal resistance

Fin Array



N = number of fins

total area of N fins

A_t = plus area of exposed base $A_{b,o}$

$$A_t = NA_f + A_{b,o}$$

$$\eta_o = 1 - N \frac{A_f}{A_t} (1 - \eta_f)$$

overall fin efficiency

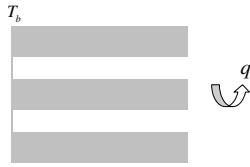
$$q = \frac{T_b - T_\infty}{R_{t,o}}$$

total rate of heat transfer from fins and exposed base

$$R_{t,o} = \frac{I}{hA_t \eta_o}$$

overall resistance

fin array w/o contact resistance



$$q = \frac{T_b - T_\infty}{R_{t,o}}$$

$$T_b \bullet \bigtriangleup \!\! \bigtriangleup \bullet T_\infty$$

$$R_{t,o} = \frac{I}{hA_t \eta_o}$$

fin array with a base w/o contact resistance



$$q = \frac{T_b - T_\infty}{R_{base} + R_{t,o}}$$

$$T_b \bullet \bigtriangleup \!\! \bigtriangleup \bullet R_{base} \bullet \bigtriangleup \!\! \bigtriangleup \bullet R_{t,o} \bullet \bigtriangleup \!\! \bigtriangleup \bullet T_\infty$$

$$R_{base} = \frac{L_{base}}{kA_b}$$

$$R_{t,o} = \frac{I}{hA_t \eta_o}$$

fin array with a base with contact resistance



$$q = \frac{T_b - T_\infty}{R_{t,c} + R_{base} + R_{t,o}}$$

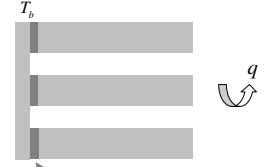
$$T_b \bullet \bigtriangleup \!\! \bigtriangleup \bullet R_{t,c} \bullet \bigtriangleup \!\! \bigtriangleup \bullet R_{base} \bullet \bigtriangleup \!\! \bigtriangleup \bullet R_{t,o} \bullet \bigtriangleup \!\! \bigtriangleup \bullet T_\infty$$

$$R_{t,c} = R_{t,c}'' / A_b$$

$$R_{base} = \frac{L_{base}}{kA_b}$$

$$R_{t,o} = \frac{I}{hA_t \eta_o}$$

fin array with contact resistance



$$q = \frac{T_b - T_\infty}{R_{t,o}}$$

$$T_b \bullet \bigtriangleup \!\! \bigtriangleup \bullet R_{t,o(c)} \bullet \bigtriangleup \!\! \bigtriangleup \bullet T_\infty$$

$$R_{t,o(c)} = \frac{I}{hA_t \eta_{o(c)}}$$

$$\eta_{o(c)} = 1 - N \frac{A_f}{A_t} \left(1 - \frac{\eta_f}{c_1} \right)$$

$$c_1 = 1 + \eta_f h A_f \frac{R_{t,c}''}{A_{c,f}}$$

fin efficiency

$$\eta_f$$

can be determined

- from figures 3.19, 3.20 (p.190)

L_c = corrected fin length applied to adiabatic boundary conditions

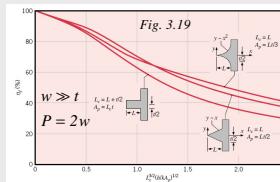


Fig. 3.19

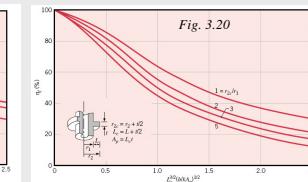


Fig. 3.20

- from Table 3.5 (p.169)

$$m = \left(\frac{2h}{kt} \right)^{1/2} \quad \text{for (a)}$$

$$m = \left(\frac{4h}{kD} \right)^{1/2} \quad \text{for (b)}$$

fin effectiveness

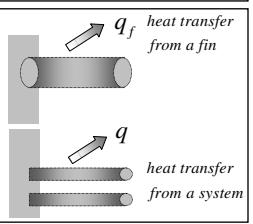
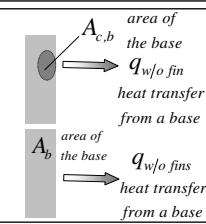
$$\varepsilon_f$$

Single Fin

$$\varepsilon_f = \frac{q_f}{q_{w/o\ fin}} = \frac{q_f}{h(T_b - T_\infty) A_{c,b}}$$

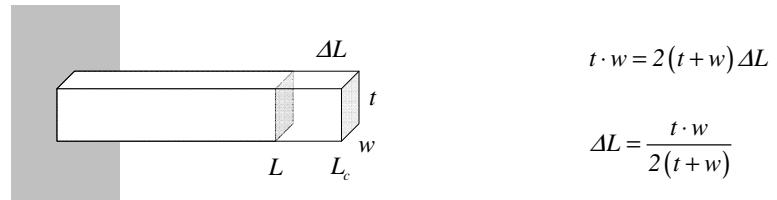
Fin Array

$$\varepsilon = \frac{q}{q_{w/o\ fins}} = \frac{q}{h(T_b - T_\infty) A_b}$$



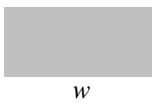
Addition to the Table 3.5 (p.152) **Efficiency of common fin shapes – Pin Fins**

Rectangular^b (all sides are included)



$$t \cdot w = 2(t+w)\Delta L$$

$$\Delta L = \frac{t \cdot w}{2(t+w)}$$

$P = 2(t+w)$  w	$L_c = L + \frac{t \cdot w}{2(t+w)}$ $A_f = 2L_c(t+w)$	$\eta_f = \frac{\tanh mL_c}{mL_c}$ $m = \sqrt{\frac{hP}{kA_c}} = \sqrt{\frac{2h(t+w)}{ktw}}$
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$t = w$ (square)  w	$P = 4w$ $A_f = 4L_c w$ $L_c = L + \frac{w}{4}$	$\eta_f = \frac{\tanh mL_c}{mL_c}$ $m = \sqrt{\frac{hP}{kA_c}} = \sqrt{\frac{4h}{kw}}$
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