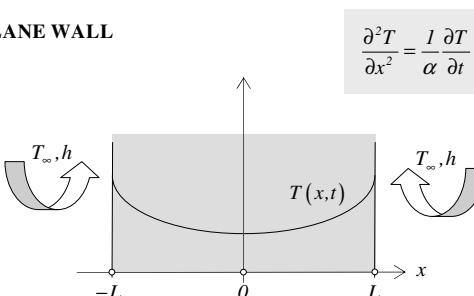
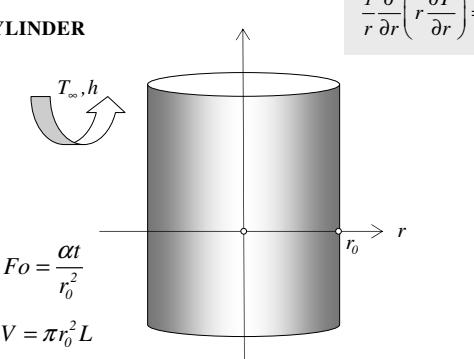
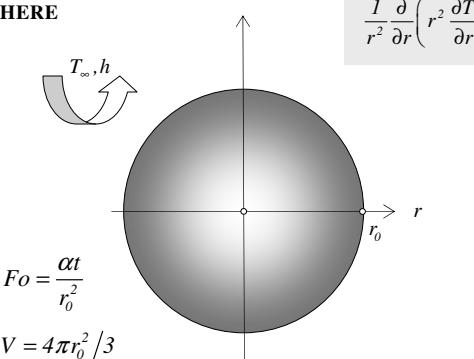


TRANSIENT CONDUCTION – APPROXIMATE ANALYTICAL SOLUTIONS

Approximation is valid for

 $Fo > 0.2$

initial temperature T_i	ambient temperature T_∞	non-dimensional temperature $\Theta^* = \frac{T - T_\infty}{T_i - T_\infty}$	non-dimensional coordinates $x^* = \frac{x}{L}$	$r^* = \frac{r}{r_0}$	non-dimensional time $Fo = \frac{\alpha t}{L^2}$	$Fo = \frac{\alpha t}{r_0^2}$
PLANE WALL						
		$\frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$				
						
$Fo = \frac{\alpha t}{L^2}$	$V = 2LWH$	$Bi = \frac{hL}{k} \quad \text{Table 5.1 p.301} \Rightarrow \varsigma_I, C_I$			$\Theta^* = C_I \cos(\varsigma_I x^*) e^{-\varsigma_I^2 Fo}$	approximate solution (one term solution)
					$T(x,t) = T_\infty + (T_i - T_\infty) C_I \cos(\varsigma_I \frac{x}{L}) e^{-\varsigma_I^2 \frac{\alpha}{L^2} t}$	approximate solution is valid for $Fo > 0.2$ or $t > 0.2 \frac{L^2}{\alpha}$
					$t = \frac{L^2}{\alpha \varsigma_I^2} \cdot \ln \left[\frac{T_\infty - T_i}{T_\infty - T(x,t)} \cdot C_I \cdot \cos(\varsigma_I \frac{x}{L}) \right]$	time needed to heat the wall at location x from T_i to a current temperature $T(x,t)$
					$Q = \left[1 - C_I \frac{\sin(\varsigma_I)}{\varsigma_I} e^{-\varsigma_I^2 \frac{\alpha}{L^2} t} \right] \cdot \rho c_p V \cdot (T_i - T_\infty)$	total heat transferred from the wall over the time t
CYLINDER						
		$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) = \frac{1}{\alpha} \frac{\partial T}{\partial t}$			$\Theta^* = C_I J_0(\varsigma_I r^*) e^{-\varsigma_I^2 Fo}$	approximate solution
					$T(r,t) = T_\infty + (T_i - T_\infty) \cdot C_I \cdot J_0 \left(\varsigma_I \frac{r}{r_0} \right) \cdot e^{-\varsigma_I^2 \frac{\alpha}{r_0^2} t}$	$J_0(x)$ is a Bessel Function (B.4 p.1017)
$Fo = \frac{\alpha t}{r_0^2}$	$V = \pi r_0^2 L$	$Bi = \frac{hr_0}{k} \quad \text{Table 5.1} \Rightarrow \varsigma_I, C_I$			$t = \frac{r_0^2}{\alpha \varsigma_I^2} \cdot \ln \left[\frac{T_\infty - T_i}{T_\infty - T(r,t)} \cdot C_I \cdot J_0 \left(\varsigma_I \frac{r}{r_0} \right) \right]$	time needed to heat the cylinder at location r from T_i to a current temperature $T(r,t)$
					$Q = \left[1 - 2C_I J_1(\varsigma_I) e^{-\varsigma_I^2 \frac{\alpha}{r_0^2} t} \right] \cdot \rho c_p V \cdot (T_i - T_\infty)$	total heat transferred from the cylinder over the time t
SPHERE						
		$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) = \frac{1}{\alpha} \frac{\partial T}{\partial t}$			$\Theta^* = C_I \frac{\sin(\varsigma_I r^*)}{\varsigma_I r^*} e^{-\varsigma_I^2 Fo}$	approximate solution
					$T(r,t) = T_\infty + (T_i - T_\infty) \cdot C_I \cdot \frac{\sin(\varsigma_I \frac{r}{r_0})}{\varsigma_I \frac{r}{r_0}} \cdot e^{-\varsigma_I^2 \frac{\alpha}{r_0^2} t}$	Note that at $r=0$ $\frac{\sin(\varsigma_I \frac{r}{r_0})}{\varsigma_I \frac{r}{r_0}} = 1$
$Fo = \frac{\alpha t}{r_0^2}$	$V = 4\pi r_0^2 / 3$	$Bi = \frac{hr_0}{k} \quad \text{Table 5.1} \Rightarrow \varsigma_I, C_I$			$t = \frac{r_0^2}{\alpha \varsigma_I^2} \cdot \ln \left[\frac{T_\infty - T_i}{T_\infty - T(r,t)} \cdot \frac{C_I \cdot \sin(\varsigma_I \frac{r}{r_0})}{\varsigma_I \frac{r}{r_0}} \right]$	time needed to heat the sphere at location r from T_i to a current temperature $T(r,t)$
					$Q = \left[1 - \frac{3C_I \cdot (\sin \varsigma_I - \varsigma_I \cdot \cos \varsigma_I)}{\varsigma_I^3} \cdot e^{-\varsigma_I^2 \frac{\alpha}{r_0^2} t} \right] \cdot \rho c_p V \cdot (T_i - T_\infty)$	total heat transferred from the sphere over the time t