

criterion for fully developed conditions

$$S = \left[\frac{Re_D \cdot Pr}{L/D} \right]^{1/3} \cdot \left[\frac{\mu}{\mu_s} \right]^{0.14}$$

$$Re_D = \frac{\rho u_m D}{\mu} = \frac{4\dot{m}}{\pi \mu D}$$

$$Nu_D = \frac{hD}{k}$$

$$h = \frac{k \cdot Nu_D}{D}$$

Developing Flow

$$S \geq 2$$

combined entry length

velocity and temperature profiles are developing simultaneously



$$(8.57) \quad \overline{Nu}_D = 1.86 \cdot \left[\frac{Re_D \cdot Pr}{L/D} \right]^{1/3} \cdot \left[\frac{\mu}{\mu_s} \right]^{0.14} = 1.86 \cdot S$$

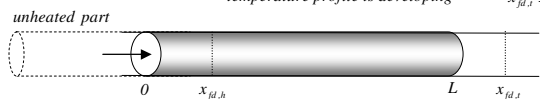
for $T_s = \text{const}$

$0.48 < Pr < 16,700$

$0.0044 < \frac{\mu}{\mu_s} < 9.75$

thermal entry length

velocity profile is developed
temperature profile is developing



$$(8.56) \quad \overline{Nu}_D = 3.66 + \frac{0.0668 \cdot \frac{Re_D \cdot Pr}{L/D}}{1 + 0.04 \left[\frac{Re_D \cdot Pr}{L/D} \right]^{2/3}}$$

for $T_s = \text{const}$

also good for large $Pr > 5$ (oils)

Fully Developed Flow

$$S < 2$$

$$\bar{h} = h_x = \text{const}$$

$$\overline{Nu}_D = Nu_D = \text{const}$$

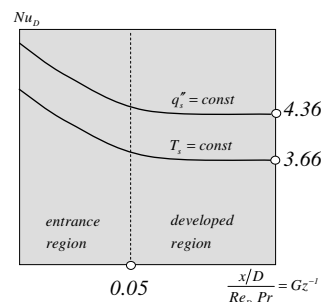
$$q_s'' = \text{const}$$

$$(8.53) \quad Nu_D = 4.36$$

$$T_s = \text{const}$$

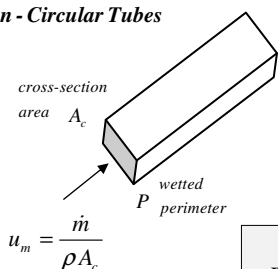
$$(8.55) \quad Nu_D = 3.66$$

$$h = \frac{k \cdot Nu_D}{D}$$



Non-Circular Tubes

Hydraulic Diameter:



$$D_h = \frac{4A_c}{P}$$

$$Re_{D_h} = \frac{\rho u_m D_h}{\mu} = \frac{4\dot{m}}{\mu P}$$

$Re_{D_h} < 2300$ laminar \Rightarrow Table 8.1

$Re_{D_h} > 2300$ turbulent \Rightarrow Use (8.61) with $Pr \geq 0.7$

TABLE 8.1 Nusselt numbers and friction factors for fully developed laminar flow in tubes of differing cross section

Cross Section	$\frac{b}{a}$	$Nu_D = \frac{hD_h}{k}$		$f Re_{D_h}$
		(Uniform q_s'')	(Uniform T_s)	
	—	4.36	3.66	64
	1.0	3.61	2.98	57
	1.43	3.73	3.08	59
	2.0	4.12	3.39	62
	3.0	4.79	3.96	69
	4.0	5.33	4.44	73
	8.0	6.49	5.60	82
	∞	8.23	7.54	96
	∞	5.39	4.86	96
	—	3.11	2.49	53

Used with permission from W. M. Kays and M. E. Crawford, *Convection Heat and Mass Transfer*, 3rd ed. McGraw-Hill, New York, 1993.