

properties at $\bar{T}_m = \frac{T_{m,i} + T_{m,o}}{2}$

μ_s at T_s

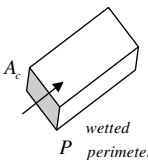
We consider long pipes for which :

$$Re_D = \frac{\rho u_m D}{\mu} = \frac{4\dot{m}}{\pi \mu D}$$

$$Nu_D = \frac{hD}{k}$$

$$h = \frac{k \cdot Nu_D}{D}$$

$$\overline{Nu}_D = Nu_D$$

for $T_s = \text{const}$ smooth pipe, small to moderate temperature difference			
Dittus (8.60)	$Nu_D = 0.023 \cdot Re_D^{4/5} \cdot Pr^n$	$n = 0.4$ if $T_s > T_m$ (heating of fluid) $n = 0.3$ if $T_s < T_m$ (cooling of fluid)	$0.7 < Pr < 160$ $Re_D > 10,000$ $L > 60D$
for $T_s = \text{const}$ or $q_s'' = \text{const}$ smooth pipe, large property variation			
Sieder (8.61)	$Nu_D = 0.027 \cdot Re_D^{4/5} \cdot Pr^{1/3} \cdot \left(\frac{\mu}{\mu_s} \right)^{0.14}$	$0.7 < Pr < 16,700$ $Re_D > 10,000$ $L > 60D$	<p>can be applied for non-circular tubes</p> <p>with $D_h = \frac{4A_c}{P}$</p> 
for $T_s = \text{const}$ or $q_s'' = \text{const}$			
Gnielinski (8.62)	$Nu_D = \frac{(f/8) \cdot (Re_D - 1000) \cdot Pr}{1 + 12.7 \cdot (f/8)^{1/2} \cdot (Pr^{2/3} - 1)}$	$0.5 < Pr < 2000$ $3000 < Re_D < 5e6$ $L > 60D$	<p>for smooth pipes (8.21):</p> $f = \frac{1}{(0.79 \ln Re_D - 1.64)^2}$ <p>for rough pipes use Moody charts</p>
Liquid Metals			
for $q_s'' = \text{const}$ smooth pipe, fully developed			
Skupinski (8.64)	$Nu_D = 4.82 + 0.0185 Pe_D^{0.287}$	$100 < Pe_D < 10000$ $3.6e3 < Re_D < 9.05e6$	$Pe_D = Re_D \cdot Pr$
for $T_s = \text{const}$			
Seban (8.65)	$Nu_D = 5.0 + 0.025 Pe_D^{0.8}$	$Pe_D \geq 100$	
Short Tubes			
(8.63)	$\overline{Nu}_D = Nu_D \cdot \left[1 + \frac{C}{(x/D)^m} \right]$	Nu_D is calculated for fully developed flow	<p>coefficients C and m depend on the shape of inlet</p> <p>Example: sharp-edged</p> 